## complete manual



INSTRUCTION MANUAL MODEL 660 GUARDED DC DIFFERENTIAL VOLTMETER

## WARRANTY

We warrant each of our products to be free from defects in material and workmanship. Our obligation under this warranty is to repair or replace any instrument or part thereof (except tubes and batteries) which, within a year after shipment, proves defective upon examination.

To exercise this warranty, contact your Keithley field engineering representative. You will be given assistance and shipping instructions.

## REPAIRS AND RECALIBRATION

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FIGURE 1. Keithley Instruments Model 660 Guarded DC Differential Voltmeter.

## SECTION I. GENERAL DESCRIPTION

## 1-1. DESCRIPTION.

a. The Keithley Model 660 Guarded DC Differential Voltmeter is a convenient, self-contained potentiometric system that accurately measures dc voltages. It has $\pm 0.02 \%$ 1imit of error from 100 millivolts to 500 volts full scale, $0.005 \%$ repeatability, and a reference supply stable to $0.005 \%$ indefinitely without manual standardization. Maximum null sensitivity is $\pm 100$ microvolts full scale; resolution is within 2 microvolts.
b. Features for convenient use include: five in-line readout dials with automatically lighted decimal points; 10 to $25-$ millivolt recorder output; input polarity switch; floating operation up to 500 volts off ground; fast overload recovery; better than 45 decibels of $60-\mathrm{cps}$ rejection.

1-2. OPERATING MODES. The Mode1 660 can be used as a potentiometer or as a conventional vacuum tube voltmeter. As a potentiometer, it can measure from 100 millivolts to 500 volts full scale with $\pm 0.02 \%$ limit of error and from 100 microvolts to 100 millivolts full scale within 20 microvolts. As a VTVM, the Model 660 can measure from 100 microvolts to 500 volts full scale with an accuracy of $\pm 3 \%$ of full scale. It can also measure resistances from 10 megohms to 50,000 megohms within $\pm 5 \%$.

## 1-3. APPLICATIONS.

a. The Model 660 is used for measurements over a wide range. Typical applications in the microvolt region are the matching of semi-conductors and the monitoring of noise, transients and drift. High level voltage applications include power supply and meter calibration, and tube potential measurements.
b. Overall stability of $0.01 \%$ indefinitely makes the Model 660 useful in measurements of extended duration. Measurements of long-term power supply stability, long-term drift runs, and monitoring during environmental and reliability tests are possible uses.
c. The null-detector output permits use with potentiometric recorders and digital voltmeters equipped with automatic print-out. The Model 660 is useful in quality control, product development, inspection and production.
d. Floating operation to 500 volts is provided for measurements such as plate potential differences of balanced amplifiers.

1-4. ACCESSORIES.
a. Model 6601A High Voltage Divider is a $100: 1$ divider which extends the range of the Model 660 to 5000 volts. The divider accuracy is $\pm 0.01 \%$ and its input resistance is 10 megohms. The overall limit of error of the Model 660 with the Model 6601 A is $\pm 0.03 \%$. Paragraph $2-5$ gives operating instructions for the Divider.
b. Model 4000 Rack Mounting Kit, containing two brackets and a top cover, adapts the Model 660 for standard 19 -inch rack mounting. For rack mounting, the Model 660 is 19 inches wide $x$ 13-1/2 inches deep x 5 inches high. Refer to paragraph 2-12 for installing instructions.

1-5. SPECIFICATIONS.

## AS AN ULTRA-STABLE POTENTTOMETER:

LIMIT OF ERROR: $\pm 0.02 \%$ of input voltage or 20 microvolts, whichever is greater, after 15 -minute warm-up.

REPEATABILITY: Within $0.005 \%$.
COMBINED STABILITY OF KELVIN-VARLEY DIVIDER AND REFERENCE VOLTAGE SUPPLY: $\pm 0.01 \%$ indefinitely, after l-hour warm-up. Temperature coefficient does not exceed $0.002 \%$ per ${ }^{\circ} \mathrm{C}$.

MAXIMUM NULL SENSITIVITY: 100 microvolts full scale with 2.0 -microvolt resolution.

INPUT RESISTANCE: Infinite at null, from 0 to 500 volts.
POLARITY: Positive or negative, selectable by switch.
FLOATING OPERATION: May be operated with up to 500 volts between $L 0$ and GND (chassis ground).

RESISTANCE - LOW TO GROUND: $10^{8}$ ohms shunted by 0.05 microfarad. RESOLJTION CHART:

| Input Voltage <br> Range <br> (volts) | Maximum Dial <br> Resolution <br> (mililivolts) | Maximum Usable <br> Full-Scale Null <br> Sensitivity <br> (millivolts) | Maximum Meter <br> Resolution <br> (microvolts) |
| :---: | :---: | :---: | :---: |
| $50-500$ | 10 | 10 | 100 |
| 5 | -50 | 1 | 1 |

AS A SENSITIVE VTVM:
Voltage Ranges (positive or negative)
Input Resistance
500 volts
50 volts
5 volts
0.5 volt

10 megohms
10 megohms
10 megohms
10 megohms

Null Ranges

## Input Resistance (Slewing)

| 100 volts | 10 megohms |
| ---: | ---: |
| 10 volts | 10 megohms |
| 1 volt | 10 megohms |
| 100 millivolts | 1 megohm |
| 10 millivolts | 1 megohm |
| 1 millivolt | 1 megohm |
| 0.1 millivolt | 100 kilohms |

NOTE: Input resistance on 0.1-millivolt range can be increased; see paragraph 2-8.

VTVM ACCURACY: $\pm 3 \%$ of full scale on all ranges.
DRIFT: Less than 10 microvolts, non-cumulative, after 15 -minute warm-up.
60 CPS REJECTION: Greater than 45 db .
GENERAL CHARACTERISTICS:
STABILITY OF REFERENCE VOLTAGE SUPPLY: $\pm 0.005 \%$ indefinitely, after 1-hour warm-up.

STABILITY OF ZENER REFERENCE: 20 ppm per year and five ppm per ${ }^{\circ} \mathrm{C}$.
LINE TRANSIENT REGULATION: Less than 5 ppm for $10 \%$ variation from 117 volts.
ACCURACY OF DIVIDER: 0.005\%.
CHARACTERISTICS OF NULL DETECTOR OUTPUT:
Output: Adjustable 10 to 25 millivolts dc full scale, all ranges. Output Resistance: 300 ohms maximum. Noise: 2 microvolts peak-to-peak (referred to input).

Note: Recorder used must have input fully isolated - $10^{10}$ ohm minimum leakage.

CONNECTORS: Input: Binding posts on front panel. Output: Banana jacks on rear.

TUBE COMPLEMENT: One OG3, five 12AX7, one 12BH7, two 12B4A, one 6CM8.
POWER: $105-125$ volts or $210-250$ volts, $50-60 \mathrm{cps}, 75$ watts.
DIMENSIONS (Bench): 5-1/2 inches high x 17-1/2 inches wide x 13-1/2 inches deep.

NET WEIGHT: 24 pounds.
1-6. EQUIPMENT SHIPPED. The Model 660 Guarded DC Differential Voltmeter is factory-calibrated and is shipped with all components in place. All units are shipped for bench use. Model 4000 Kit may be ordered for rack mounting; refer to paragraph 2-12 for assembly instructions. The shipping carton also contains the Instruction Manual.


FIGURE 2. Model 660 Front Panel Controls and Terminals. Designations refer to Parts List.


FIGURE 3. Model 660 Rear Controls and Terminals.

## SECTION 2. OPERATION

2-1. FRONT PANEL CONTROLS AND TERMINALS. (See Figure 2.)
a. POLARITY Switch. The POLARITY Switch turns the instrument on and selects the input polarity. The Switch reverses the polarity of the internal reference voltage supply so both positive and negative voltages may be measured; it does not reverse the meter polarity.
b. NULL Switch. The NULL Switch sets the null detector sensitivity for seven decade ranges from 0.1 millivolt to 100 volts full scale. When the Switch is in the VTVM position, the Model 660 operates as a conventional vacuum tube voltmeter for the four ranges of the RANGE Switch.
c. RANGE Switch. The RANGE Switch adjusts the sensitivity of the VTVM in four steps: $0.5,5,50$ and 500 volts full scale. It also determines the voltage across the Kelvin-Varley divider and the position of the decimal point light - which also serves as a pilot light - between the five Reference Voltage Dials.
d. Reference Voltage Dials. Five in-1ine dials at the top of the front panel set the reference voltage when the Model 660 is used as a potentiometer.
e. METER ZERO Control. The METER ZERO Control adjusts the meter pointer to zero. The control is needed on only the 0.1 and $1.0-\mathrm{millivolt}$ null ranges; on the other ranges, the pointer will normally be on zero without adjustment. The control has a range of approximately $\pm 50$ microvolts.
f. Input Terminals. At the lower left front panel, the black LO terminal is to be connected to the low impedance terminal of the unknown voltage and the red HI terminal is to be connected to the high impedance terminal. A second set of terminals marked LO and GND is provided for grounding the LO input terminal to the chassis when desired. The LO terminals are connected together internally.

2-2. REAR CONTROLS AND TERMINALS. (See Figure 3.)
a. Fuse. For 105-125 volt operation, the Model 660 uses a 1-ampere 3 AG fuse. For 210-250 volt operation, the Model 660 uses a 0.5 -ampere 3 AG fuse.
b. Power Cord. The Model 660 is for a $105-125$ volt, $50-60 \mathrm{cps}$ line source, unless otherwise specified on the rear panel. A three-wire power cord is used.
c. NULL DETECTOR OUTPUT. Two terminals, marked + and -, supply a dc signal from the null detector.
d. OUTPUT ADJUST. A screwdriver control next to the OUTPUT terminals adjusts the null detector output between 10 and 25 millivolts full scale.

2-3. PRELIMLNARY PROCEDURES.
a. Connect the Model 660 power cord to a $105-125$ volt, $50-60 \mathrm{cps}$ line
source. Set the controls as follows:

| RANGE | 500 |
| :--- | :--- |
| NULL | VTVM |
| POLARITY | + |
| Reference Voltage Dials | Zero |

The decimal light between the third and fourth dials will light. Allow the instrument to warm up for 15 minutes to meet the specified accuracy on all ranges.
b. With the input terminals open, set the NULL Switch to 0.1 MV and zero the meter with the METER ZERO Control. The stability of the Model 660 is such that no adjustment should be required in eight hours after a 15 -minute warm-up. Then return the NULL Switch to VTVM.

2-4. OPERATING PROCEDURES.
a. The Model 660 is used first as a VTVM to determine the approximate value of the unknown voltage. It is then used in the potentiometric mode to determine the voltage to $\pm 0.02 \%$.
b. VTVM Operating Procedures.

1. Eleven full-scale ranges are available for VTVM operation. When the NULL Switch is at VTVM, the RANGE Switch determines one of four full-scale ranges. By putting the five Reference Voltage Dials at zero, the Model 660 can then operate as a VTVM on the seven null ranges.
2. Connect the unknown voltage to the input terminals, using the LO terminal for the low impedance terminal of the unknown. Refer to Figure 4.


FIGURE 4. Input Connections to Model 660. The two diagrams show the input circuit for measuring at ground and for floating.

In A, the unknown voltage has one terminal at ground. The shorting link is between the LO and GND terminals of the Model 660 .

In B, the unknown voltage has both terminals off ground potential. Note this floating or off-ground potential must be less than 500 volts. Also note the shorting link is not used.
3. Switch the RANGE Switch to the most sensitive range for an on-scale meter deflection.
c. Potentiometric Operating Procedures.

NOTE
Avoid large overload voltages on the null detector. No permanent damage will occur even with 500 -volt overloads, but some open circuit offset will be caused in the null detector. The offset, due to the polarization of the input filter capacitors, will disappear after about an hour.

1. Leave the RANGE Switch at the last setting used in the VTVM operation. If the VTVM reading is negative, reverse the POLARITY Switch.
2. Set the first two Reference Voltage Dials to the first two digits of the unknown voltage found in the VTVM operation.
3. Set the NULL Switch to the initial null setting shown in Table 1. Adjust the Voltage Reference Dials progressively for zero meter deflection while increasing the null detector's sensitivity with the NULL Switch. Deflections to the right indicate the voltage being measured is more positive than the Reference Voltage Dial setting.

| RANGE | Initial NULL <br> Setting | Most Sensitive <br> NULL Setting |
| :---: | :---: | :---: |
| 500 volts | 100 volts | 10 millivolts |
| 50 volts | 10 volts | 1.0 millivolt |
| 5 volts | 1 volt | 0.1 millivolt |
| 0.5 volt | 100 millivolts | 0.1 millivolt |

TABLE 1. Recommended Null Sensitivities and Settings.
NOTE
The most accurate resistors in the Kelvin-Varley divider are in the first two Reference Voltage Dials. Therefore, to obtain the most accurate readings, use the first two dials whenever possible.
4. The value of the unknown voltage is read directly from the Reference Voltage Dials.
a) The Dial reading will be within the specified limit of error if the NULL Switch is at the most sensitive setting (Table l) for the range used and if the meter is as close to null as possible. The meter need not be actually at null.
b) For Dial settings below $4999 \overline{10}$, only the five Dials need be read to be within specifications. However, the meter may be read as an approximation of a sixth digit.
c) For Dial settings above $4999 \overline{10}$, the first Dial is not used and the voltage is read directly from the remaining four Dials.
d) Use the meter as a null indicator when balancing voltages. For Dial settings above 499910, the meter approximates a fifth dial reading. However, the loading effect of the Kelvin-Varley divider on the meter causes some quantative inaccuracies when the meter is off null. (See paragraph 2-8).

2-5. MODEL 6601A HIGH VOLTAGE DIVIDER.
a. The Model 6601A extends the range of the Model 660 to 5000 volts full scale. The ratio of the Divider is $100: 1, \pm 0.01 \%$; the input resistance is 10 megohms. The limit of error when the Model 660 is used with the Model 6601 A is $\pm 0.03 \%$.

## NOTE <br> Maximum input into the Model 6601A is 5000 volts.

b. Set the Model 660 RANGE Switch to 50 volts. The meter will read to 5000 volts full scale. Connect the HI and LO Divider terminals to the HI and 10 Voltmeter terminals, respectively. Connect the unknown voltage to the Divider INPUT, and use the Model 660 as outlined in paragraph 2-4.


FIGURE 5. Model 6601A High Voltage Divider.
2-6. RECORDER OUTPUT.
a. Reconmended recorders for use with the Model 660 are the F.L. Moseley Autograf 680 series recorder and the Minneapolis Honeywell recorder ( $10 \mathrm{mv}-0-10 \mathrm{mv}$ scale, 50 kilohms input resistance). Any recorder used must be able to float 500 volts off ground and its input must be fully isolated ( $10^{10} \mathrm{ohm}$ minimum leakage resistance to ground).
b. Before attaching the recorder, set all Reference Voltage Dials to zero. Disconnect the unknown voltage and short both Model 660 input terminals. Set the NULL Switch to 10 MV . Connect the recorder to the OUTPUT terminals on the Model 660 rear panel.
c. Set the Reference Voltage Dials to 10 millivolts to apply an accurate $10-m i l l i v o l t$ potential to the null detector on the $10-\mathrm{millivolt}$ null range. This will provide a full-scale recorder output which can be matched to the recorder's range between 10 and 25 millivolts by adjusting the OUTPUT ADJUST Control.
d. To obtain accurate results and/or to prevent damage to the instruments, the recorder mast be able to float off-ground with the Model 660. Leakage and pickup between the two instruments should also be minimized.

1. Make sure neither recorder terminal is grounded. Use a 3-wire grounded power line for the recorder. If a 2 -wire line is used, connect the recorder chassis and the Model 660 chassis with a separate lead.
2. Minimize all sources of leakage between the output terminals, the recorder and ground. Use polystyrene or Teflon-insulated wire where possible. If the connecting wires are shielded, connect the shield to the $L O$ terminal.
3. Avoid long leads between the Model 660 and the recorder.
4. If difficulty is encountered in off-ground measurements, such as unstable readings, connect a 10 -microfarad capacitor between the $L O$ and GND terminals on the Model 660 front panel.

NOTE
Do not short either Model 660 output terminal to the case; this may damage the Kelvin-Varley divider.
e. If there is substantial recorder jitter on the 0.1-millivolt null range, place a filter between the Model 660 and the recorder. Refer to Figure 6 for this connection. Note the filter must also be insulated from ground.


FIGURE 6. Recorder Filter. A filter between the Model 660 and the recorder may be necessary when using the 0.1-millivolt null detector range.

## 2-7. MEASURING RESISTANCES.

a. Procedures: The Model 660 can be used to rapidly measure resistances from 10 megohms to 50,000 megohms with an accuracy of $\pm 5 \%$. To measure resistance, connect the resistor across the Model 660 HI and LO terminals. Use a short isolated lead to the HI terminal to prevent measuring leakage between the leads. Set the RANGE Switch to 500 . Then determine the value of the resistor as follows:

1. For resistances between 10 megohms and 100 megohms, set the NULL Switch to 10 volts; adjust the Reference Voltage Dials to obtain a full-scale meter deflection. Subtract 10.000 from the dial setting to obtain the value of the resistor in megohms.
2. For resistances between 100 megohms and 1,000 megohms, set the NULL Switch to 1 volt; adjust the Reference Voltage Dials to obtain a full-scale meter deflection. Subtract 1.0000 from the dial setting and multiply the difference by ten to obtain the value of the resistor in megohms.
3. For resistances between 1,000 megohms and 50,000 megohms, set the NULL Switch to 1 volt; adjust the Reference Voltage Dials to obtain a convenient deflection on the meter. Calculate the value of the resistor using,

$$
R_{x}=\frac{10 E_{d}}{V} \text { megohms }
$$

Eq. 1
Where $R_{x}$ is the unknown resistance;
Ed is the Reference Voltage Dial setting in volts;
V is the null detector meter reading in volts.


FIGURE 7. Simplified Model 660 Circuit for Measuring Resistances. $R_{x}$ is the unknown resistance. $R_{n}$ is the input resistance of the null detector; $V$ is the null detector; $E_{d}$ is the buckout voltage.
b. Theory: The above method for determining the value of an unknown resistor is based upon the equation for the circuit (see Figure 7). If an unknown resistance is across the Model 660 input terminals, then

$$
\begin{equation*}
E_{d}=i\left(R_{x}+R_{n}\right) \tag{Eq. 2}
\end{equation*}
$$

where $E_{\mathrm{d}}$ is the Reference Voltage Dial setting in volts;
$i$ is the current in the circuit;
$\mathrm{R}_{\mathrm{x}}$ is the unknown resistance;
$R_{n}$ is the input resistance of the null detector meter in ohms.
The current can be written $i=V / R_{n}$, where $V$ is the null detector meter reading in volts. Equation 2 now becomes

$$
\begin{equation*}
R_{x}=R_{n}\left(\frac{E_{d}}{V}\right)-R_{n} \tag{Eq. 3}
\end{equation*}
$$

If measurements are made on the 1 to 100 -volt null ranges, the input resistance, $R_{n}$, is 10 megohms. Equation 3 becomes

$$
R_{x}=10^{7}\left(\frac{E_{d}}{V}-1\right)
$$

Eq. 4

## 2-8. EFFECTS DUE TO KELVIN-VARLEY OUTPUT RESISTANCE.

a. When the Model 660 is used for nulling on the $0.1-\mathrm{millivolt}$ range, the last Reference Voltage Dial may appear to be inaccurate. The apparent error is due to a voltage drop across the Kelvin-Varley divider. This effect involves only the null detector sensitivity and not the accuracy of the dial setting. When the Model 660 is as near to null as possible, the Reference Voltage Dial setting is correct within the instrument's specifications. There is no error at null.
b. The effect is most apparent on the 0.1 -millivolt null range. A 0.1millivolt off-null setting of the reference voltage will not produce a fullscale deflection on the meter. The output resistance of the Kelvin-Varley divider is significant compared to the shunt resistance across the null detector meter, and the IR drop across the divider will cause the meter to be in error from $1 \%$ to $38 \%$. On the 100 , 10 and $1-m i l l i v o l t$ null ranges, a setting of 100,10 and 1 millivolt off-null respectively, can show up as an error of up to $6 \%$ for Reference Voltage Dial settings near 25000 . The effect cannot be observed on the other null ranges of the Model 660.
c. The amount of deflection on the meter is equal to the ratio

$$
\frac{R_{n}}{R_{n}+R_{k v}}
$$

where $R_{n}$ is the shunt resistance across the meter ( 10 megohms for the 100 to l-volt null ranges, 1 megohm for the 100 to 1 -millivolt null ranges, and 100 kilohms for the $0.1-\mathrm{millivolt}$ null range);
$R_{k v}$ is the output resistance of the Kelvin-Varley divider, which is a maximum of 62.4 kilohms at settings of 24545 and 25455 and a minimum of 100 ohms at settings of 49998 and 00002.
d. The input resistance on the 0.1 -millivolt range may be increased by substituting a 1 -megohm, 1/2-watt resistor (Keithley Part No. R12-1M) for the 100 -kilohm input resistor, R1003, if the source resistance is not more than

100 kilohms. The higher input resistor will increase the input noise of the instrument open circuited only. The effect of line transients will also be more apparent.

## 2-9. LOADING AND OFF-NULL RESISTANCE.

a. The input resistance of the voltmeter for the seven null ranges varies from 10 megohms to 100 kilohms as given in the Specifications. This resistance, however, is not the effective input resistance of the Model 660. Its input resistance is considerably higher due to the potentiometric principle of operation. The value is given by

$$
\begin{equation*}
R_{i n}=\frac{E_{d} R_{n}}{V} \tag{Eq. 5}
\end{equation*}
$$

where $R_{\text {in }}$ is the effective input resistance of the Model 660;
$\mathrm{E}_{\mathrm{d}}$ is the voltage indicated on the Reference Voltage Dials;
$R_{n}$ is the shunt resistance or input resistance of the null detector meter;
V is the null detector meter reading.
b. To find the loading effect the Model 660 will have on a circuit, equation 5 may be used to compute the effective input resistance of the instrument. At null, the input resistance is infinite. Off null, the input resistance is usually high compared to the internal resistance of the unknown voltage, and the loading will not be enough to affect the accuracy of the measurement. For example, the Model 660 input resistance is $10^{10}$ ohms if the Reference Voltage Dials are set at 1.0000 volt on the $1-m i l l i v o l t$ null range for a reading off null by $10 \%$ of full scale.

2-10. THERMAL EMF PRECAUTIONS, Observe standard thermocouple techniques to reduce thermal emf errors for measurements using the most sensitive null ranges. Since the Model 660 can read to 0.5 microvolt, thermal emf's can introduce considerable errors into the measurements. In general, use pure copper leads throughout the system when measuring in the microvolt range. For extensive measurements in the microvolt region, request the article, DC Microvolt Measurements, from Keithley Instruments, Inc.

2-11. AC EFFECTS ON MEASUREMENTS. To minimize errors from ac signals present in the unknown voltage, the Model 660 employs a chopper-stabilized null detector operating at a $42-\mathrm{cps}$ chopping rate with a two-section $\mathrm{R}-\mathrm{C}$ filter at the input. Very large ac components on the measuring lines, however, may reduce off-null sensitivity. Also, heavy $60-\mathrm{cps}$ pickup will be observed as needle quiver. If ac components affect measurements by the Model 660, additional filtering is required. For an ac signal of a single frequency, a twin $T$ filter is effective. For an ac variable frequency, an ordinary low-pass filter may be used.

## 2-12. RACK MOUNTING. (See Figure 8.)

a. The Model 660 is shipped for bench use with four feet and a tilt-bail. The Model 4000 Rack Mounting Kit converts the instrument to rack mounting to the standard EIA (RETMA) 19-inch width.
b. To convert the Model 660 , remove the four screws at the bottom of each side of the instrument case. Lift off the top cover assembly with the handles;
save the four screws. To remove the feet and tilt bail from the bottom cover assembly, turn the two screws near the back. The two pawl-type fasteners will release the cover and allow it to drop off. Remove the feet and the tilt bail and replace the cover (2).
c. Attach the pair of rack angles (3) to the cabinet with the four screws (4) previously removed. Insert the top cover assembly (1) in place and fasten to the chassis with the two pawl-type fasteners at the rear. Store the top cover with handles, feet and tilt-bail for future use.

| $\begin{gathered} \text { Item, } \\ \text { (See Fig. 8) } \end{gathered}$ | Description | Keith1ey <br> Part No. | Quantity |
| :---: | :---: | :---: | :---: |
| 1 | Cover Assembly | 14623B | 1 |
| 2 | Cover Assembly, Bottom (Supplied with Model 660) | 14590B | 1 |
| 3 | Angle, Rack | 14624B | 2 |
| 4 | Screw, Slot Head, 10-32 UNC- $2 x 1 / 4$ <br> (Supplied with Model 660) | --- | 4 |
| 5 | Front Panel (Supplied with Model 660) | --- | 1 |

TABLE 2. Parts List for Model 4000 Rack Mounting Kit.


FIGURE 8. Exploded View for Rack Mounting.

2-13. PLACING IN RACK. The Model 660, once converted for rack mounting, easily fits into the rack. It is recommended, however, that a blower be used in the rack enclosure in which the Model 660 is mounted. The instrument specifications state a $0.002 \%$ per ${ }^{\circ} \mathrm{C}$ temperature coefficient. A temperature rise of $5{ }^{\circ} \mathrm{C}$ ( $9{ }^{\circ} \mathrm{F}$ ) will cause a $0.01 \%$ error.

2-14. 234-VOLT OPERATION. The Mode1 660 can be quickiy and easily converted to operate from a $234-v o l t$ line source. It is normally supplied with the power transformer primary windings connected in parallel for 117 -volt operation. To convert, reconnect the primary windings in series as shown on the schematic diagram: the brown lead to the black-white. Replace the l-ampere fuse with a 0.5 -ampere fuse. Power line frequency can be 50 to 400 cps for either voltage.

## SECTION 3. CIRCUIT DESCRIPTION

3-1. GENERAL. The Model 660 Differential Voltmeter measures voltage by the potentiometric method. The ultra-stable 500 -volt reference voltage supply (see Figure 9) is used with the 5-dial Kelvin-Varley divider to null the unknown voltage. The difference between the divider output and the unknown voltage is indicated by the null detector - a chopper-stabilized vacuumtube voltmeter. At null the unknown voltage equals the reference voltage and can be directly read from the five in-line dials of the Kelvin-Varley divider. The input and null detector are fully guarded to avoid leakage.

NOTE
The circuit designations referred to in the following paragraphs are for the schematic diagram 15199 H found at the back of this manual.


FIGURE 9. Simplified Circuit Diagram of the Model 660.
3-2. REFERENCE POWER SUPPLY.
a. Unregulated voltage from the transformer T 3001 is rectified by a silicon half-wave rectifier, D3004, and is filtered by capacitors C3003, C3004 and C3005. The voltage then is applied to the preregulator series pass tube, V3005.
b. The output voltage of V 3005 is regulated by comparing a sample voltage from divider string, R3015, R3016 and R3017, to the reference, regulator tube V3007. The difference between the two potentials is amplified by V3006. The amplifier output drives the grid of $V 3005$ in the proper phase to nullify input variations. The ac feedback loop, containing capacitor C3007, is used for better high frequency and transient response.
c. The regulated output of V3005 is applied to the second series tube, V3004, for final regulation. To obtain a stable, accurate voltage, the 500 -volt output of V3004 is sampled by a divider network of wirewound resistors, R3034, R3036, R3037, R3049 and R3050. The divider network ratio is adjusted with potentiometer R3035 to better than 0.01\%. Light modulator E3002 compares the sample voltage from the divider network to the voltage across the ultra-stable zener diode, D3009. Any difference between the sampled voltage and the voltage of D3009 is chopped by E3002 and amplified by a two-stage ac-coupled amplifier, V3001. The amplified output of V3001 is converted to a dc signal by light modulator, E3001, and then is amplified by the two-stage differential dc amplifier, V3002 and V3003. The amplifier output is applied to the grid of the series tube, V3004, in the proper phase to nullify input variations. Capacitor C3009 is used in the ac feedback circuit.
d. The temperature-compensated zener diode, D3009, was used as the circuit's basic reference since typical variations are limited to less than 20 ppm per year and 5 ppm per ${ }^{\circ} \mathrm{C}$. Thus, a highly stable reference is provided with respect to both time and temperature. The zener diode will also withstand extreme shock and vibration.
e. The regulated 500 volts from $V 3004$ either is applied directly to the Kelvin-Varley divider or it is divided to 50 , 5 , or 0.5 volts by very stable wirewound resistor networks. The RANGE Switch, S3002, determines which network is used. The $50-$ volt range divider network consists of R3040, R3041 and R3042; the 5-volt, of R3040, R3044 and R3045; and the 0.5-volt, of R3040, R3047 and R3048. Potentiometers R3041, R3044 and R3047 are used to accurately set the voltage division on each range.

## 3-3. KELVIN-VARLEY DIVIDER.

a. The Kelvin-Varley divider precisely divides the reference voltage for nulling an unknown voltage. It is, in effect, a constant input impedance decade potentiometer consisting of resistors R 3051 through R3099. The resistors within each decade are matched; the decades are matched for each instrument.
b. Each decade of the Kelvin-Varley divider, except the first, R3051, through R3056, parallels two resistors of the preceeding string. Between the two contacts of the first Reference Voltage Switch, S3003, the total resistance is 40 kilohms ( 80 kilohms in parallel with the 80 kilohms total resistance of the four remaining strings). With the RANGE Switch set at 500,100 volts dc will appear across the contacts of Reference Voltage Switches S3004, 10 volts across $S 3005,1$ volt across $S 3006$, and 0.1 volt across S 3007 .

## 3-4. NULL DETECTOR.

a. The Model 660 uses a null detector with a chopper stabilized, feedback amplifier. The input signal is attenuated, if necessary, and sent through a two-stage R-C filter. The signal is then amplified and measured by the null detector meter.
b. The null detector has basically three full-scale sensitivities, 0.1, 1 and 10 millivolts. Above the 10 millivolt range, the input is divided by resistors R1002 through R1007 to the $10-\mathrm{millivolt}$ level. The full-scale sensitivities are determined by which of three feedback resistors, R1037, R1038 or R1039, is in the circuit. A two-stage R-C filter, consisting of

R1008, C1001, R1009 and Cl002, is used to decrease the ac input components. The input filter attenuation ratio is 35 db at 60 cps . The light modulators are driven by a $42-\mathrm{cps}$ multi-vibrator. Using a drive source harmonically unrelated to the standard line frequency minimizes $60-\mathrm{cps}$ pickup effects.
c. The light modulators E1001 and E1002 convert the difference between the filtered input voltage and the output of the Kelvin-Varley divider into an ac voltage, which is fed to a four-stage ac coupled amplifier, V1001 and V1002. The output of the amplifier is then demodulated by light modulator E1003 and applied to an R-C filter, R1034 and C1017. The null detector meter, M1001, indicates the value of the filtered signal.
d. One arm of the feedback network is formed by resistors R1043, R1040, R1041, R1042 and one of the feedback range resistors, R1037, R1038 or R1039. Resistor R1036 forms the second shunt arm. The feedback is applied to light modulator E1002. The low end of C 1001 is also returned to the feedback point for faster speed of response.
e. A zero-control network is across resistor R1009 to buck out thermal emf's at the input on the two most sensitive ranges. The network consists of a 1.32 -volt mercury battery, BT1001, and resistors R1010 through R1013. The zero control on the front panel, R1013, has approximately a 100 -microvolt span.
f. The null detector output is obtained across resistors R1040 and R1043, which are in the feedback network. Potentiometer R1043 adjusts the output from 10 to 25 millivolts at full scale. The output voltage is proportional to the full-scale meter reading.

3-5. GUARDING. Guarding is accomplished by floating the null detector and the input circuitry at a voltage equal to the input voltage from a low impedance source. This full guarding eliminates leakage between the input terminal and ground. Such leakage in an unguarded circuit is difficult to avoid, even under laboratory conditions, and can result in sizeable errors. For example, in an unguarded circuit with a l-megohm source, leakage of $10^{8}$ ohms will introduce $0.1 \%$ error. A guarded circuit eliminates this element of error. The effectiveness of guarding in the Model 660 is demonstrated by setting the null detector on the 0.1 -millivolt range, with the input circuit open, and the Reference Voltage Dials set to 500 volts. Even at this extreme condition there is no deflection on the meter, demonstrating there is no leakage.

## SECTION 4. MAINTENANCE

4-1. GENERAL.
a. Section 4 contains the maintenance, troubleshooting and calibration procedures for the Model 660. It is recomended that these procedures be followed as closely as possible to maintain the accuracy and stability of the instrument.
b. The Model 660 needs no periodic maintenance beyond the normal care required of high-quality electronic equipment. Occasional verification of the limit of error should show if adjustments or calibration are needed.

4-2. PARTS REPLACEMENT. The Replaceable Parts List is Section 5 describes the electrical components in the Model 660. Replace components only as necessary, and use only reliable replacements which meet the specifications. Replace the resistors in the Kelvin-Varley divider, switches S3004 through S3007, only with Keithley matched resistors.

4-3. TROUBLESHOOTING.
a. The following procedures give instructions for repairing troubles which might occur in the Model 660. Use these procedures to troubleshoot and use only specified replacement parts. Table 3 lists equipment recommended for troubleshooting. If the trouble cannot be readily located or repaired, contact Keithley Instruments or its representatives.
b. Paragraph 2-12 describes how to remove the Model 660 cover. Before proceeding with the troubleshooting, check the vacuum tubes in the instrument. Normally, replacing tubes will clear up the difficulty. All tubes can be readily tested on a grid-modulated tube tester. If replacing a tube does not correct the trouble, continue the procedures. Replacing tubes does not necessitate recalibration of the instrument.
c. Table 4 contains the more comnon troubles which might occur with the instrument. If the repairs indicated in the table do not clear up the trouble, the difficulty will have to be found through a point-by-point check of the circuits. Refer to the circuit description in Section 3 to find the more crucial components and to determine their function in the circuit. The complete circuit schematic, Diagram 15199H, is found in Section 5.

| Instrument | Use |
| :--- | :--- |
| Keithley Model 503 Milliohmeter | Ohnmeter for resistors less than $1 \mathrm{k} \Omega$ |
| Keithley Model 610A Electrometer | Dc voltmeter and ohmmeter |
| Keithley Model 662 Guarded dc |  |
| Differential Voltmeter | Test Kelvin-Varley divider resistors |
| Grid-modulated tube tester | Test vacuum tubes |

TABLE 3. Equipment Recommended for Troubleshooting Model 660. Use these instruments or their equivalents.

| Difficulty | Probable Cause | Solution |
| :---: | :---: | :---: |
| Poor null meter sensitivity on millivolt ranges. | C1018 or R1046 out of adjustment. | Adjust per paragraph 4-4. |
| Needle quiver. | R1046 is out of adjustment. | Adjust per paragraph 4-4. |
| Meter rattle, drift or error is observed on all null ranges. | Tube V1001, V1002 or V2001 is faulty. | Check tube; replace if faulty. |
| Variations in line voltages cause Model 660 measurements to be out of specifications. | Tube V3005, V3006 or V3007 is defective. | Check tube; replace if faulty. |
| Reference voltage supply drifts, requiring frequent adjusting of the range controls, R3035, R3041, R3044, R3048. | $\begin{aligned} & \text { V3001, V3002, V3003 or V3007 } \\ & \text { is defective. } \end{aligned}$ | Check tubes; replace if faulty. |
|  | One of the divider resistors, R3034 through R3037, R3049 or R3050, is changing value rapidly during warm-up. | Test the resistors and replace any faulty components. |
|  | Zener reference diode, D3009, is unstable. | Check zener diode per paragraph 4-5. Replace if faulty. |
|  | Light modulator E3002 is defective. | Check light modulator by replacing. |
| Measurements out of tolerance on the 500 -volt range. | Out of calibration. | Refer to paragraph 4-8 for recalibration. |
|  | One of the divider resistors, R3034 to R3037, R3049 or R3050, is faulty. | Check stability for 24 hours. If 500 -volt supply remains stable, replacement of resistors is not needed. |

TABLE 4 (Sheet l). Model 660 Troubleshooting.

| Difficulty | Probable Cause | Solution |
| :--- | :--- | :--- |
| Measurements out of tolerance <br> on the 500-volt range. | Noisy or unstable zener ref- <br> erence diode, D3009. | Check zener diode. Replace if faulty. |
| Measurements are out of <br> specifications on one range <br> other than 500-volt range. | A resistor in the range <br> divider network is faulty. | Paragraph 3-2 e points out the resistors <br> used for each range. Try to bring the <br> ranges within specification by calibra- <br> ting with the potentiometers in the net- <br> work. See paragraph 4-8. If it does <br> not work, check individual resistors. |
| Measurements are out of <br> specifications on all ranges <br> other than 500-volt range. | Resistor R3040 is faulty. | Replace the faulty resistor. |
| Measurements are out of <br> specifications on any range <br> when the Reference Voltage <br> Dials are at any setting <br> other than 499910. | One of the Kelvin-Varley <br> divider resistors is <br> faulty. | See paragraph 4-7. |
| Instrument is out of <br> specifications on all <br> ranges. | One of resistors R1001 <br> through R1007 is faulty. | Check resistors; replace if faulty. |

## 4-4. ADJUSTMENT OF HUM BALANCING CONTROLS.

a. Adjusting Trimmer C1018.

1. Trimmer C1018 nulls out residual ac components in the power transformer, T3001. If this adjustment is not properly set, null sensitivity decreases. On the 0.1 -millivolt null range, however, it is normal to have a maximum sensitivity of $62 \%$ of full scale when the Reference Voltage Dials are set near 25000. This is due to the loading of the null detector by the Kelvin-Varley divider (paragraph 2-8).


FIGURE 10. Attaching Oscilloscope Leads for Adjusting Trimmer. The oscilloscope is attached to the LO input terminal and the guard circuit.
2. To adjust the trimmer, remove the bottom cover and attach an oscilloscope between the LO input terminal and the guard circuit (see Figure 10). With the Reference Voltage Dials set for either 24545 or 25455 , the wave form should be similar to that shown in Figure 11. Adjust trimmer 01018 (Figure 19) until the wave form is correct.

## NOTE

Trimmer C1018 and resistor R1045 are normally used in each instrument. In some instruments, however, component parameters are such that this adjustment is unnecessary and C1018 and R1045 are disconnected at manufacture.


FIGURE 11. Wave Forms for Adjusting Trimmer. The wave form with C1018 properly adjusted is shown in (a). The wave form with trimmer misadjusted is shown in (b). A Tektronix Type 503 Oscilloscope was used; horizontal sweep was $20 \mathrm{msec} / \mathrm{cm}$; vertical, $10 \mathrm{mv} / \mathrm{cm}$.

## b. Adjusting HUM BAL Potentiometer R1046.

1. Potentiometer Rl046 minimizes $60-\mathrm{cps}$ pickup in the null detector. Misadjustment will reduce sensitivity and cause needle quiver.
2. To adjust the potentiometer, set the Reference Voltage Dials to zero and short the input terminals. Attach an oscilloscope to the junction of capacitor Cl014 and resistor Rl034 (from pin 6 of V1002). Figure 12 shows the wave form if potentiometer R1046 is adjusted for minimum output.


FIGURE 12. Wave Form with R1046 Adjusted. A Tektronix Type 503 Oscilloscope was used; horizontal sweep was $20 \mathrm{msec} / \mathrm{cm}$; vertical, $500 \mathrm{mv} / \mathrm{cm}$.

4-5. ZENER CURRENT TEST. When the reference voltage supply is operating properly, the zener current will be 10 milliamperes and the voltage across R3031 should be 100 millivolts.

## 4-6. CALIBRATION PROCEDURES.

a. The following procedures are recommended for calibrating the Model 660. Use the equipment recommended in Table 5. If proper facilities - especially important for calibrating an $\pm 0.02 \%$ instrument - are not available or if difficulty is encountered, contact Keithley Instruments or its representatives to arrange for factory calibration.
b. Three procedures are covered: Kelvin-Varley divider verification, voltage range calibration, and reference voltage supply stability test.
c. If the Model 660 is not within specifications after the calibrations, follow the troubleshooting procedures or contact Keithley Instruments or its representatives.

| Instrument | Use |
| :---: | :---: |
| Electro Scientific Industries Model | Range Voltage Calibrator |
| SV-194B Voltage Calibrator, $\pm 0.005 \%$ accuracy with corrections on certificate |  |
| Electro Scientific Industries Model | Voltage divider for range cali- |
| RV-722 Kelvin-Varley Divider, linearity: settings of 0.1 to 1 , Certificate Corrected to $\pm 0.2 \mathrm{ppm}$ | bration |
| Keithley Instruments Model 150A Microvoltmeter | Null detector for range calibration |
| Keithley Instruments Model 241 Regulated High Voltage Supply | Power supply for range calibration |
| Keithley Instruments Model 662 Guarded DC Differential Voltmeter | Check voltages in Kelvin-Varley divider |
| Mosley Instruments Model 680 Direct Reading Recorder | Recorder for reference voltage supply stability |
| Weston Instruments Model 3 Type 7 Saturated Standard Cell | Range calibration and reference voltage supply stability |
| Weston Instruments Model 66 Oil Bath | Range calibration and reference voltage supply stability |

TABLE 5. Recommended Equipment for Model 660 Calibration. Use these instruments or their equivalents.

4-7. KELVIN-VARLEY DIVIDER VERIFICATION.
a. There is no in-field calibration for the Kelvin-Varley divider; its accuracy can only be verified. The divider accuracy depends upon matching resistors and switches. At manufacture, each resistor within the first two Reference Voltage switches, S3003 and S3004, is matched to $\pm 0.005 \%$. The resistors in the switches are checked as a set to an accuracy of better than $0.005 \%$. Individual resistors
cannot be replaced without rematching the entire divider deck.
b. Kelvin-Varley Divider Accuracy Verification Procedures.

1. Use the Model 662 Differential Voltmeter or equipment with better limit of error to match the Model 660 under test. Connect the wiper arm of Switch S3007 of the instrument under test to the HI terminal of the Model 662. Connect both LO terminals.

NOTE
Be careful of high voltages when working within the Model 660. Up to 900 volts dc is present at various points.
2. Set the dials to random settings on both instruments. Settings should match to $\pm 0.02 \%$. This procedure, however, only indicates the Kelvin-Varley divider accuracy. The errors of the two instruments may be additive, causing a false verification. The Most accurate way is to use standard procedures for checking a Kelvin-Varley divider or to return the Model 660 to the factory.
3. If any resistor fails to test out, the entire divider string will have to be rematched.

## 4-8. RANGE CALIBRATION.

a. The reference voltage supply has a 500 -volt output which can be attenuated to 50,5 or 0.5 volts. This voltage is then divided by the KelvinVarley divider to provide the accurate buckout voltage. Each of the four voltage ranges is set by internally adjusting potentiometers R3035, R3041, R3044 and R3048 (Figure 15).
b. The ranges are calibrated by applying an accurate voltage to the Model 660 for each setting of the RANGE Switch. The Model 660 is set to furnish the equivalent buckout voltage, and the internal range potentiometer is adjusted until the voltmeter indicates a null.

NOTE
The accuracy of the Model 660 calibration will be no greater than the accuracy of the voltage source used for calibrating. Unless the user is familiar with techniques for obtaining greater accuracy than $0.01 \%$ ( 100 ppm ), it is better to return the Model 660 to the factory for range calibration.
c. The most critical part in range calibration is establishing a reference source whose accuracy exceeds $0.01 \%$. Use the Model SV-194B Voltage Calibrator for the $500,50,5$ and 0.5 -volt outputs. Establish the accuracy of these outputs by determining the corrections for the calibrator's CALIBRATION and OUTPUT dials at these outputs. The system's accuracy can be determined to approximately 10 ppm . Added to the accuracy of the standard cell, total accuracy should be approximately 20 ppm . Note, this will depend upon properly executed procedures.
d. Procedures to Establish System Accuracy.

1. Set up the system shown in Figure 13. Use the 9.9 -megohm extender for only the 0.5 and 5-volt outputs. Have the Model SV-194B certified by the manufacturer to accuracy.
2. Establish the corrections for the CALIBRATION dial setting for Model SV-194B outputs of $500,50,5$ and 0.5 volts. Set the Power Supply (preferably, the Model 241 which is $0.05 \%$ accurate) to 500 volts. Set the Kelvin-Varley Divider to a voltage equal to that of the standard cell. Adjust the Model SV-194B ratio dial until the Null Detector indicates a null. The difference between the settings of the Kelvin-Varley Divider and the ratio dial is the Model SV-194B correction factor at 500 volts. With this correction, the 500 volts may be set to within 20 ppm .
3. Connect the Null Detector to the 50,5 and 0.5 -volt taps of the Model SV-194B Calibrator in that order. Set the Kelvin-Varley Divider to corresponding voltages. Use the 9.9 megohm extender for the 5 and 0.5 volt outputs. (See Figure 13.) The difference read on the Null Detector is the correction factor for each of the three voltages. These voltages may also be set to within 20 ppm .
4. Use the four correction factors for calibrating the Model 660 range settings.


FIGURE 13. Block Diagram to Establish System Accuracy for Model. 660 Range Calibration. Fully guard the entire system to prevent leakage errors. Use a l-kilohm copper resistor to shunt the Null Detector. See Table 5 for recommended equipment.


FIGURE 14. Block Diagram for Model 660 Range Calibration. Fully guard entire system to prevent leakage errors. See Table 5 for recommended equipment.
e. Procedures for Range Calibration.

1. Set up the system shown in Figure 14. The standard cell should be certified to 10 ppm. Use the dial correction factors found for each output. If the system accuracy was properly determined, the input voltage to the Model 660 should be correct to 20 ppm .
2. 500-volt Range Calibration: Set the Model 660 as follows:

RANGE 500
Reference Voltage Dials $499.9 \overline{10}$
NULL VTVM
POLARITY
Adjust the Voltage Calibrator to apply 500 volts dc to the Model 660. Turn the Model 660 NULL Switch to 10 MV and adjust the 500 V CAL potentiometer R3035 (Figure 15) for null on the Model 660.
3. 50-Volt Range Calibration: Set the Model 660 as follows:

RANGE 50
Reference Voltage Dials $49.99 \overline{10}$
NULL 10 MV
POLARITY
$+$
Adjust the Voltage Calibrator to apply 50 volts de to the Model 660. Adjust the 50 V CAL potentiometer R3041 (Figure 15) for an off-null reading on the Model 660 equal to the correction factor at 50 volts.
4. 5-Volt Range Calibration: Set the Model 660 as follows:

$$
\begin{array}{ll}
\text { RANGE } & 5 \\
\text { Reference Voltage Dials } & 4.999 \overline{10} \\
\text { NULL } & 1 \mathrm{MV} \\
\text { POLARITY } & +
\end{array}
$$

Adjust the Voltage Calibrator to apply 5 volts dc to the Model 660. Adjust the 5 V CAL potentiometer R 3044 (Figure 15) for an off-nu11 reading on the Model 660 equal to the correction factor at 5 volts.
5. 0.5-Volt Range Calibration: Set the Model 660 as follows:

RANGE
0.5

Reference Voltage Dials . $4999 \overline{10}$
NULL
POLARITY
0.1 MV
$+$

Adjust the Voltage Calibrator to apply 0.5 volt de to the Model 660. Adjust the 0.5 V CAL potentiometer R 3047 (Figure 15) for an off-null reading on the Model 660 equal to the correction factor at 0.5 volt.


FIGURE 15. Model 660 Internal Controls. (Top View.)


FIGURE 16. Circuit Diagram for Reference Voltage Supply Stability Test. The voltage across the 250 -ohm resistor is slightly higher than the standard cell. Use the $10-\mathrm{kilohm}$ potentiometer to shunt the divider voltage down. All resistors are wirewound. See Table 5 for recommended equipment.

4-9. REFERENCE VOLTAGE SUPPLY STABILITY TEST.
a. The reference voltage supply, consisting of the power transformer, the main supply (printed circuit PC55), and the reference section (printed circuit PC61), is factory calibrated for an output of 500 volts dc $\pm .005 \%$. Its stability is $\pm 0.005 \%$ indefinitely after a 1 -hour warm-up. The 500 -volt output is adjustable to meet specifications. If the stability of the supply is not within specifications, then troubleshooting for a faulty component or replacing the supply is probably required.
b. Routine calibration of the Model 660 does not require a stability test of the reference voltage supply. However, a stability test is recommended if one of the components in the supply is replaced.
c. For the 24 -hour test, the 500 -volt output of the reference voltage supply is divided and compared to a $1.02-v o l t$ saturated standard cell using a sensitive null detector. Variations between the reference voltage supply and the standard cell are detected by the Model 150A and are recorded on a recorder. Refer to Figure 16 for the block diagram of the test circuit.
d. In using the test circuit, the following points are important.

1. Saturated standard cells, though extremely stable with time, have a high temperature coefficient and require a controlled environment during use. Therefore, the Weston Oil Bath, which is maintained at $+35^{\circ} \mathrm{C} 50.05^{\circ} \mathrm{C}$, is used for the test. Unsaturated standard cells have a lower temperature coefficient, but they do not have the long term stability required for this test.
2. The resistor divider network is constructed from wire of the same spool for an extremely close temperature coefficient match ( 4 ppm , typically). Additional stability results when the resistors are immersed in an oil bath to hold the ambient temperature variations to $\pm 0.01 \%$.

## e. Procedures for the Reference Voltage Supply Stability Test.

1. After the saturated standard cell and the resistor divider network are placed in the oil bath and connected to the circuit, allow sufficient time for the cell to stabilize at $+35^{\circ} \mathrm{C}$. (Consult Keithley Instruments for details.) Set the Model 660 controls as follows:

| RANGE | 500 |
| :--- | :--- |
| Reference Voltage Dials | 499.910 |
| NULL | 10 MV |
| POLARITY | OFF |

Connect the resistor divider network across the Model 660's reference voltage supply, the positive side of the divider input to the wiper arm of the last Reference Voltage Switch, S3007, and the negative side of the divider to the LO terminal on the Model 660 front panel.
2. Connect the Model 150A and the recorder as shown in Figure 16. Set the Model 150A to the 3 -volt range. Advance the Model 660 POLARITY Switch to + to put 500 volts across the divider. If the Model 150 A reads two volts, the standard cell and the divider voltages are improperly connected in series. If the circuit is correct, the Model 150A will read zero. Increase the Model 150A's sensitivity to the 0.1 -millivolt range. If it reads more than 20 microvolts, adjust the $10-\mathrm{kilohm}$ potentiometer shunting the divider.

## NOTE

Any adjustment of potentiometer R3035 requires all other ranges be calibrated.
3. After a 1 -hour warm-up, the drift of the entire system should not exceed $\pm 50$ microvolts in 24 hours (Figure 17).


FIGURE 17. Stability Strip Chart for Model 660 Reference Voltage Supply. The chart covers over 15 hours. Fluctuations are well within $\pm 0.005 \%$. Note drift is non-cumulative. No compensation for variations of line voltage or other conditions was made.


FIGURE 18. Top View of Model 660 Chassis. Location of components and printed circuits is shown above. Refer to Parts List for circuit designations.


FIGURE 19. Bottom View of Model 660 Chassis. Location of components is shown in the figure. Refer to Parts List for circuit designations.


FIGURE 20. Resistor Locations on Printed Circuit 54. Other components are shown in Figure 21. Refer to Parts List for circuit designations.


FIGURE 21. Battery, Capacitor, Modulator, Diode and Tube Locations on Printed Circuit 54. Resistors are shown in Figure 20.


FIGURE 22. Resistor Locations on Printed Circuit 55. Other components are shown in Figure 23.


FIGURE 23. Capacitor, Modulator, Diode and Tube Locations on Printed Circuit 55. Resistors are shown in Figure 22.


FIGURE 24. Resistor Locations on Printed Circuit 36. Resistor R1049 is not used in the Model 660.


FIGURE 25. Component Locations on Printed Circuit 61. The values of resistors R3049 and R3050 are determined at factory calibration.


FIGURE 26. Model 6601A Component Locations.

## SECTION 5. REPLACEABLE PARTS

5-1. REPLACEABLE PARTS LIST. The Replaceable Parts List describes the components of the Models 660 and 6601A. The List gives the circuit designation, the part description, a suggested manufacturer and the Keithley Part Number. The last column indicates the figure picturing the part. The name and address of the manufacturers listed in the "Mfg. Code" column are contained in Table 7.

5-2. HOW TO ORDER PARTS.
a. For parts orders, include the instrument's model and serial number, the Kefthley Part Number, the circuit designation and a description of the part. A11 structural parts and those parts coded for Keithley manufacture (80164) must be ordered from Keithley Instruments, Inc. In ordering a part not listed in the Replaceable Parts List, completely describe the part, its function and its location.
b. Order parts through your nearest Keithley distributor or the Sales Service Department, Keithley Instruments, Inc.

| amp | ampere | MtF | Metal Film |
| :---: | :---: | :---: | :---: |
| CbVar | Carbon Variable | Mil. No. | Military Type Number |
| CerD | Ceramic, Disc | My | Mylar |
| Comp | Composition |  |  |
|  |  | $\Omega$ | ohm |
| DCb | Deposited Carbon |  |  |
|  |  | Poly | Polystyrene |
| EMC | Electrolytic, metal cased | p | pico (10-12) |
| ETB | Electrolytic, tubular |  |  |
| ETT | Electrolytic, tantalum | $\mu$ | micro ( $10^{-6}$ ) |
| £ | farad | v | volt |
| k | kilo (10 ${ }^{3}$ ) | Var | Variable |
|  |  | w | watt |
| M or meg | mega ( $10^{6}$ ) or megohms | WW | Wirewound |
| m | milli ( $10^{-3}$ ) | WWVar | Wirewound Variable |
| Mfg. | Manufacturer |  |  |

TABLE 6. Abbreviations and Symbols.

MODEL 660 REPLACEABLE PARTS LIST
(Refer to Schematic Diagram 15199H for circuit designations)
CAPACITORS

| Circuit <br> Desig. | Value | Rating | Type | Mfg. <br> Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Cl001}$ | $1.0 \mu \mathrm{f}$ | 600 v | MtF | 13050 | C12-1.0M | 21. |
| C1002 | $1.0 \mu \mathrm{f}$ | 600 v | MtF | 13050 | C12-I.0M | 21 |
| C1003 | . $05 \mu \mathrm{f}$ | 600 v | My | 56289 | C62-.05M | 21 |
| C1004 | $80 \mu \mathrm{f}$ | 350 v | EMC | 53021 | C32-80M | 21 |
| C1005 | $200 \mu \mathrm{f}$ | 3 v | EMC | 14655 | C48-200M | 21 |
| C1006 | $10 \mu f$ | 15 v | ETB | 56289 | C3-10M | 21 |
| C 1007 | . $1 \mu \mathrm{f}$ | 600 v | MtF | 02777 | C47-0.1M | 21 |
| C1008 | . $05 \mu \mathrm{f}$ | 600 v | My | 56289 | C62-.05M | 21 |
| C1009 | 40/20 $\mu \mathrm{f}$ | 450 v | EMC | 56289 | C36-40/20M | 21 |
| C1010 | $.047 \mu \mathrm{f}$ | 1000 v | Poly | 96733 | C67-.047M | 19 |
| C1011 | . $002 \mu \mathrm{f}$ | 600 v | CerD | 72982 | C22-.002M | 21 |
| $\mathrm{Cl012}$ | $10 \mu \mathrm{E}$ | 15 v | ETB | 56289 | C3-10M | 21 |
| C1013 | . $1 \mu \mathrm{f}$ | 600 v | MtF | 02777 | C47-0.1M | 21 |
| C1014 | . $25 \mu \mathrm{f}$ | 400 v | M 5 F | 13050 | C73-. 25 M | 21 |
| C 1015 | $100 \mu \mathrm{f}$ | 15 v | ETB | 56289 | C3-100M | 21 |
| C1016 | $4 \mu \mathrm{f}$ | 250 v | EMC | 14655 | C27-4M | 21 |
| C1017 | $560 \mu \mathrm{f}$ | 6 v | ETT | 12065 | C95-560M | 21 |
| C1018 | $1.5 / 7 \mathrm{pf}$ | 500 v | Trimmer | 71590 | C76-1.5/7P | 19 |
| C2001 | Not Used |  |  |  |  |  |
| C 2002 | . $022 \mu \mathrm{f}$ | 400 v | MtF | 13050 | C73-.022M | 23 |
| C2003 | . $022 \mu \mathrm{f}$ | 400 v | MtF | 13050 | C73-.022M | 23 |
| C3001 | . $001 \mu \mathrm{f}$ | 600 v | CerD | 72982 | C22-.001M | 19 |
| C3002 | $1000 \mu \mathrm{f}$ | 15 v | EMC | 56289 | C4-1000M | 23 |
| C3003 | $20 \mu \mathrm{f}$ | 450 v | EMC | 37942 | C36-20M | 23 |
| C3004 | $20 \mu \mathrm{f}$ | 450 v | EMC | 37942 | C36-20M | 23 |
| C3005 | 20/40 $\mu \mathrm{f}$ | 450 v | EMC | 56289 | C36-40/20M | 23 |
| C 3006 | 330 pf | 600 v | CerD | 72982 | C22-330P | 23 |
| C3007 | . $01 \mu \mathrm{f}$ | 2000 v | CerD | 56289 | C88-.01M | 23 |
| C3008 | . $01 \mu \mathrm{f}$ | 600 v | CerD | 72982 | C22-.01M | 23 |
| C3009 | $1.0 \mu \mathrm{f}$ | 1000 v | MtF | 13050 | C14-1.0M | 23 |
| C3010 | . $05 \mu \mathrm{f}$ | 600 v | My | 56289 | C62-.05M | 23 |
| C3011 | $4 \mu \mathrm{f}$ | 250 v | EMC | 14655 | C27-4M | 23 |
| C3012 | $50 \mu \mathrm{f}$ | 6 v | EMC | 56289 | C17-50M | 23 |
| C3013 | . $0047 \mu \mathrm{f}$ | 600 v | Cerd | 01121 | C22-.0047M | 23 |
| C3014 | . $022 \mu \mathrm{f}$ | 200 v | MtF | 13050 | C6-.022M | 25 |
| C3015 | . $05 \mu \mathrm{f}$ | 1600 v | My | 14655 | C87-.05M | 19 |

DIODES

| Circuit <br> Desig. | Type | Number | Mfg. Code | Keithley Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D1001 | Not Used |  |  |  |  |
| D1002 | Not Used |  |  |  |  |
| D1003 | Silicon | 1N645 | 01295 | RF-14 | 21 |
| D1004 | Silicon | 1N645 | 01295 | RF-14 | 21 |
| D3001 | Silicon | 1N3256 | 02735 | RF-22 | 21 |
| D3002 | Not Used |  |  |  |  |
| D3003 | Not Used |  |  |  |  |
| D3004 | Silicon | 1N2378 | 08520 | RF-25 | 23 |
| D3005 | Silicon | 1N3256 | 02735 | RF-22 | 23 |
| D3006 | Silicon | 1NI563A | 04713 | RF-19 | 23 |
| D3007 | Silicon | 1N1563A | 04713 | RF-19 | 23 |
| D3008 | Zener | 1N1601 | 81483 | DZ-9 | 23 |
| D3009 | Zener | G3440 | 81483 | D2-8 | 25 |

MLSCELLANEOUS PARTS

| Circuit Desig. | Description | Mfg. <br> Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: |
| BT1001 | ```Battery, 1.32-volt Mercury (Mfg. No. PX13T2)``` | 37942 | BA-12 | 21 |
| DS2001 | Neon Pilot Light (Mfg. No. NE-2P) | 08804 | PL-2 |  |
| DS2002 | Neon Pi.lot Light (Mfg. No. NE-2P) | 08804 | PL-2 |  |
| DS2003 | Neon Pilot Light (Mfg. No. NE-2P) | 08804 | PL-2 |  |
| DS2004 | Neon Pilot Light (Mfg. No. NE-2P) | 08804 | PL-2 |  |
| E1001 | Light Modulator | 80164 | 1510 | 21 |
| E1002 | Light Modulator | 80164 | 1510 | 21 |
| E1003 | Light Modulator | 80164 | 1511 | 21 |
| E3001 | Light Modulator | 80164 | 1510 | 23 |
| E3002 | Light Modulator | 80164 | 1510 | 25 |
| F1001 (117v) | Fuse, 1.0 amp , 3 AG (Mfg. No. MDL) | 71400 | FU-10 | 3 |
| F1001 (234v) | Fuse, $0.5 \mathrm{amp}, 3 \mathrm{AG}$ (Mfg. No. MDL) | 71400 | FU-6 | 3 |
| --- | Fuse Holder (Mfg. No. 34201) | 75915 | FH-3 |  |
| J1001 | Binding Post, HI (Mfg. No. DF31RC) | 58474 | BP-8R | 2 |
| J1002 | Binding Post, LO (Mfg. No. DF31BC) | 58474 | BP-8B | 2 |
| J1003 | Binding Post, LO (Mfg. No. DF31BC) | 58474 | BP-8B | 2 |
| J1004 | Binding Post, GND (Mfg. No. DF31BC) | 58474 | BP-8B | 2 |
| --- | Shorting Link (Mfg. No. 938-L) | 24655 | BP-6 |  |
| --- | Banana Jack, Red, NULL DETECTOR OUTPUT (Mfg. No. 108-745-1) | 74970 | BJ-3 | 3 |

MISCELLANEOUS PARTS (Cont'd)

| Circuit Desig. | Description | Mfg. Code | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: |
| --- | Banana Jack, Black, NULL DETECTOR OUTPUT (Mfg. No. 108-745-2) | 74970 | BJ-4 | 3 |
| M1001 | Meter | 80164 | ME-38 | 18 |
| P1001 | Line Cord (Mfg. No. 4638-13) | 82879 | CO-2 | 3 |
| --- | Clamp | 80164 | CC-7 |  |
| S1001 | Rotary Switch, Assembly less components, NULL | 80164 | 15135B | 19 |
| --- | Switch Assembly with components, NULL | 80164 | 15136B |  |
| --- | Skirted Knob Assembly, Null Switch | 80164 | 15110A |  |
| S3001 | Rotary Switch less components, POLARITY | 80164 | SW-119 | 19 |
| --- | Switch Assembly with components, POLARITY | 80164 | 15138B |  |
| --- | Skirted Knob Assembly, Polarity Switch | 80164 | 14838A |  |
| S3002 | Rotary Switch less components, RANGE | 80164 | SW-116 | 19 |
| --- | Switch Assembly with components, RANGE | 80164 | 15137B |  |
| --- | Skirted Knob Assembly, Range Switch | 80164 | 14838A |  |
| - | Skirted Knob Assembly, Meter Zero Potentiometer | 80164 | 14838A |  |
| S3003 | Switch Assembly with components, Readout | 80164 | 14869B | 2 |
| --- | Dial Assembly, 0-4 Readout | 80164 | 14827A |  |
| S3004 | Switch Assembly with components, Readout | 80164 | 15114B | 2 |
| --- | Dial Assembly, 0-9 Readout | 80164 | 14828A |  |
| S3005 | Switch Assembly with components, Readout | 80164 | 15112B | 2 |
| --- | Dial Assembly, 0-9 Readout | 80164 | 14828A |  |
| S3006 | Switch Assembly with components, Readout | 80164 | 15111B | 2 |
| --- | Dial Assembly, 0-9 Readout | 80164 | 14828A |  |
| S3007 | Switch Assembly with components, Readout | 80164 | 15115B | 2 |
| --- | Dial Assembly, 0-10 Readout | 80164 | 14829A |  |
| T3001 | Transformer | 80164 | TR-50 | 18 |

## RESISTORS

| Circuit <br> Desig. | Value | Rating | Type | Mfg. <br> Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| R1001 | $10 \mathrm{M} \Omega$ | $1 \%, 1 / 2 \mathrm{w}$ | DCb | 79727 | $\mathrm{R} 12-10 \mathrm{M}$ | 24 |
| R1002 | $1.25 \mathrm{M} \Omega$ | $1 \%, 1 / 2 \mathrm{w}$ | MtF | 75042 | $\mathrm{R} 61-1.25 \mathrm{M}$ | 24 |
| R1003 | $100 \mathrm{k} \Omega$ | $1 \%, 7 \mathrm{w}$ | WW | 91637 | $\mathrm{R} 43-100 \mathrm{~K}$ | 24 |
| R1004 | $9010 \Omega$ | $1 \%, 1 / 2 \mathrm{w}$ | DCb | 79727 | Rl2-9010 | 24 |
| R1005 | $93 \mathrm{k} \Omega$ | $1 \%, 1 / 2 \mathrm{w}$ | DCb | 79727 | R12-93K | 24 |

RESISTORS (Cont'd)

| $\begin{aligned} & \text { Circuit } \\ & \text { Desig. } \end{aligned}$ | Value | Rating | Type | Mfg. <br> Code | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1006 | 1.11 M | 1\%, 1/2 w | DCb | 79727 | R12-1.11M | 24 |
| R1007 | $1 \mathrm{k} \Omega$ | 1\%, $1 / 2 \mathrm{w}$ | DCb | 79727 | R12-1K | 24 |
| R1008 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-100K | 20 |
| R1009 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-100K | 20 |
| R1010 | $5 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-5K | 20 |
| R1011 | $5 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-5K | 20 |
| R1012 | 5 M | 1\%, 1/2 w | DCb | 79727 | R12-5M | 20 |
| R1013 | $10 \mathrm{k} \Omega$ | 10\%, 2 w | WWVar | 12697 | RP27B-10K | 19 |
| R1014 | 1 M | 10\%, 1/2 w | Comp | 01121 | R1-1M | 20 |
| R1015 | 1 M | 10\%, 1/2 w | Comp | 01121 | R1-1M | 20 |
| R1016 | $10 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-10K | 20 |
| R1017 | $1.5 \mathrm{M} / 2$ | 10\%, 1/2 w | Comp | 75042 | R61-1.5M | 20 |
| R1018 | $330 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-330K | 20 |
| R1019 | 1.5 M | 10\%, 1/2 w | Comp | 01121 | R1-1.5M | 20 |
| R1020 | $15 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-15K | 20 |
| R1021 | 10 M | 10\%, 1/2 w | Comp | 01121 | R1-10M | 20 |
| R1022 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-100K | 20 |
| R1023 | *100 k $\Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-100K | 24 |
| R1024 | * 1 M | 1\%, 1/2 w | DCb | 79727 | R12-1M | 24 |
| R1025 | Not Used |  |  |  |  |  |
| R1026 | 10 m | 10\%, 1/2 w | Comp | 01121 | R1-10M | 20 |
| R1027 | $8.2 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-8.2K | 20 |
| R1028 | $1.5 \mathrm{M} / 2$ | 10\%, 1/2 w | Comp | 01121 | R1-1.5M | 20 |
| R1029 | $1 \mathrm{M} /$ | 10\%, 1/2 w | Comp | 01121 | R1-1M | 20 |
| R1030 | 3.3 M | 10\%, 1/2 w | Comp | 01121 | R1-3.3M | 20 |
| R1031 | $1.2 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-1.2K | 20 |
| R1032 | $100 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-100K | 20 |
| R1033 | $220 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-220K | 20 |
| R1034 | $6.8 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-6.8K | 20 |
| R1035 | $1 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-1K | 20 |
| R1036 | $2 \mathrm{k} \Omega$ | 1\%, 1 w | WW | 15909 | R58-2K | 20 |
| R1037 | * $40 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-40K | 24 |
| R1038 | * $400 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-400K | 24 |
| R1039 | $4 \mathrm{M} / 2$ | 1\%, 1/2 w | DCb | 79727 | R12-4M | 24 |
| R1040 | $80 \Omega$ | 1\%, 1 w | WW | 15909 | R58-80 | 20 |
| R1041 | $500 \Omega$ | 10\%, 5 w | WWVar | 71450 | RP3-500 | 20 |
| R1042 | $1.5 \mathrm{k} \Omega$ | 1\%, 1 w | WW | 15909 | R58-1.5K | 20 |
| R1043 | $200 \Omega$ | 10\%, 2 w | WWVar | 71450 | RP22-200 | 18 |
| R1044 | $10 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-10K | 19 |
| R1045 | *10 M | 10\%, 1/2 w | Comp | 01121 | RI-10M | 19 |

[^0]MODEL 660 DIFFERENTIAL VOLTMETER

## RESISTORS (Cont'd)

| Circuit Desig. | Value | Rating | Type | Mfg. Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1046 | $1 \mathrm{k} \Omega$ | 20\%, 0.2 w | CbVar | 71450 | RP31-1K | 20 |
| R1047 | $113.6 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-113.6K | 24 |
| R1048 | 100 M 2 | 20\%, 1/2 w | Comp | 75042 | R37-100M | 19 |
| R2001 | $180 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-180K | 22 |
| R2002 | $150 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | RI-150K | 22 |
| R2003 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-270K | 22 |
| R2004 | $1 \mathrm{M} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-1M | 22 |
| R2005 | $22 \mathrm{k} \Omega$ | 10\%, 2 w | Comp | 01121 | R3-22K | 22 |
| R2006 | $22 \mathrm{k} \Omega$ | 10\%, 2 w | Comp | 01121 | R3-22K | 22 |
| R2007 | $1 \mathrm{M} /$ | 1\%, 1/2 w | DCb | 79727 | R12-1M | 22 |
| R2008 | *52 k | 1\%, 1/2 w | DCb | 79727 | R12-52K | 22 |
| R2009 | $150 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-150K | 22 |
| R2010 | $180 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-180K | 22 |
| R2011 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-270K | 22 |
| R2012 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-270K | 22 |
| R2013 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-270K | 22 |
| R2014 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | RI-270K | 22 |
| R3001 | $220 \Omega$ | 10\%, 1/2 W | Comp | 01121 | R1-220 | 22 |
| R3002 | $100 \mathrm{k} \Omega$ | 10\%, 2 w | Comp | 01121 | R3-100K | 22 |
| R3003 | 1 M | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3004 | 1 M | 10\%, 1/2 w | Comp | 01121 | RI-1M | 22 |
| R3005 | $1 \mathrm{M} /$ | 10\%, I/2 w | Comp | 01121 | R1-1M | 22 |
| R3006 | $1 \mathrm{M} / 2$ | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3007 | $5 \Omega$ | 3\%, 25 w | WW | 91637 | R30-5 | 18 |
| R3008 | $470 \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-470 | 22 |
| R3009 | $150 \mathrm{k} \Omega$ | 10\%, 2 w | Comp | 01121 | R3-150K | 22 |
| R3010 | $75 \mathrm{k} \Omega$ | 10\%, 1 w | Comp | 01121 | R2-75K | 22 |
| R3011 | $33 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-33K | 22 |
| R3012 | $220 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-220K | 22 |
| R3013 | 2.2 M | 10\%, I/2 w | Comp | 01121 | R1-2.2M | 22 |
| R3014 | 1 M | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3015 | $600 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-600K | 22 |
| R3016 | $600 \mathrm{k} \Omega$ | 1\%, $1 / 2 \mathrm{w}$ | DCb | 79727 | R12-600K | 22 |
| R3017 | $166.7 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-166.7K | 22 |
| R3018 | $470 \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-470 | 22 |
| R3019 | $470 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-470K | 22 |
| R3020 | $1 \mathrm{M} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3021 | $1 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-1K | 22 |
| R3022 | $4.7 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-4.7K | 22 |
| R3023 | 1 M | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3024 | 10 M | 10\%, 1/2 w | Comp | 01121 | RI-10M | 22 |
| R3025 | $150 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-150K | 22 |

[^1]RESISTORS (Cont'd)

| Circuit Desig. | Value | Rating | Type | Mfg. Code | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R3026 | $680 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-680K | 22 |
| R3027 | $270 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-270K | 22 |
| R3028 | 2.2 M | 10\%, 1/2 w | Comp | 01121 | R1-2.2M | 22 |
| R3029 | $5.6 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-5.6K | 22 |
| R3030 | $65.4 \mathrm{k} \Omega$ | 0.1\%, 50 w | WW | 91637 | R73-65.4K | 18 |
| R3031 | $100 \Omega$ | 0.1\%, 1 w | WW | 15909 | R70-100 | 22 |
| R3032 | $1 \mathrm{M} /$ | 10\%, 1/2 w | Comp | 01121 | R1-1M | 22 |
| R3033 | $220 \mathrm{k} \Omega$ | 10\%, 1/2 w | Comp | 01121 | R1-220K | 25 |
| R3034 | $125 \mathrm{k} \Omega$ | 0.1\%, 2 w | WW | 80164 | 15436A-125K | 25 |
| R3035 | $200 \Omega$ | 10\%, 5 w | WWVar | 71450 | RP3-200 | 25 |
| R3036 | $125 \mathrm{k} \Omega$ | 0.1\%, 2 w | WW | 80164 | 15436A-125K | 25 |
| R3037 | * $4 \mathrm{k} \Omega$ | 0.1\%, 1/4 w | WW | 80164 | 15436A-4K | 25 |
| R3038 | $200 \Omega$ | 1\%, $1 / 2 \mathrm{w}$ | DCb | 79727 | R12-200 |  |
| R3039 | $1.8 \mathrm{k} \Omega$ | 1\%, 1/2 w | DCb | 79727 | R12-1.8K |  |
| R3040 | $250 \mathrm{k} \Omega$ | 0.1\%, 2 w | WW | 80164 | 15432A-250K | 22 |
| R3041 | $1 \mathrm{k} \Omega$ | 10\%, 5 w | WWVar | 71450 | RP3-1K | 22 |
| R3042 | $32.32 \mathrm{k} \Omega$ | 0.1\%, 1/2 w | WW | 80164 | *** |  |
| R3043 | $18 \mathrm{k} \Omega$ | 1\%, $1 / 2 \mathrm{w}$ | DCb | 79727 | R12-18K |  |
| R3044 | $1 \mathrm{k} \Omega$ | 10\%, 5 w | WWVar | 71450 | RP3-1K | 22 |
| R3045 | $2.563 \mathrm{k} \Omega$ | 0.1\%, 1/2 w | WW | 80164 | \%ek* |  |
| R3046 | $187 \mathrm{k} \Omega$ | 1\%, $1 / 2 \mathrm{w}$ | DCb | 79727 | R12-187K |  |
| R3047 | $1 \mathrm{k} \Omega$ | 10\%, 5 w | WWVar | 71450 | RP3-1K | 22 |
| R3048 | $250.9 \Omega$ | 0.1\%, 1/2 w | WW | 80164 | **** |  |
| R3049 | * | 0.1\%, 1/4 w | WW | 01686 | R95-* | 25 |
| R3050 | * | 0.1\%, 1/4 w | WW | 01686 | R95-* | 25 |
| R3051 to |  |  |  |  |  |  |
| R3057 to |  |  |  |  |  |  |
| R3067\%* | $8 \mathrm{k} \Omega$ | 0.02\%, l w | WW | 80164 | \% $\% 16318 \mathrm{~A}-8 \mathrm{~K}$ |  |
| R3068 to |  |  |  |  |  |  |
| ...R3078\%* | $1.6 \mathrm{k} \Omega$ | 0.05\%, 1/2 w | WW | 80164 | **16318A-1.6K |  |
| R3079 to |  |  |  |  |  |  |
| R3089R3090 to |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| R3099 | $64 \Omega$ | 0.1\%, 1/2 w | WW | 15909 | R67-64 |  |
| *Nominal value, factory selected |  |  |  |  |  |  |
| *These resistors supplied only as complete matched sets. |  |  |  |  |  |  |
| *hi*Resistors designated R3042, R3045 and R3048 are supplied only as Resistor Set 14857A. |  |  |  |  |  |  |

VACUUM TUBES

| Circuit Desig. | Number | Mfg. Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: |
| V1001 | 12AX7 | 73445 | EV-12AX7 | 21 |
| V1002 | 6CM8 | 00011 | EV-6CM8 | 21 |
| V2001 | 12BH7 | 85599 | EV-12BH7 | 23 |
| V3001 | 12AX7 | 73445 | EV-12AX7 | 23 |
| V3002 | 12AX7 | 73445 | EV-12AX7 | 23 |
| V3003 | 12AX7 | 73445 | EV-12AX7 | 23 |
| V3004 | 12B4A | 85599 | EV-12B4A | 23 |
| V3005 | 12B4A | 85599 | EV-12B4A | 23 |
| V3006 | 12AX7 | 73445 | EV-12AX7 | 23 |
| V3007 | OG3 | 73445 | EV-0G3 | 23 |

MODEL 6601A REPLACEABLE PARTS LIST
(Refer to Schematic Diagram 16321B for circuit designations)

TERMLNALS

| Circuit Desig. | Description |  | Mfg. Code | Keithley <br> Part No. |
| :---: | :---: | :---: | :---: | :---: |
| J101 | Receptacle, hn modified |  | 80164 | CS-79 |
| -- | Plug, hn, Mate of J101, No. 7908) | Mil. No. UG-59A/U (Mfg. | 91737 | CS-80 |
| J102 | Binding Post, HI OUTPUT | (Mfg. No. DF31RC) | 58474 | BP-8R |
| J103 | Binding Post, LO OUTPUT' | (Mfg. No. DF31BC) | 58474 | BP-8B |

## RESISTORS

| Circuit Desig. | Value | Rating | Type | Mfg. <br> Code | Keithley <br> Part No. | Fig. <br> Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R101 | $2 M$ | 0.1\%, 1 w | WW | 54294 | R91-2M | 26 |
| R102 | 2 M | 0.1\%, 1 w | WW | 54294 | R91-2M | 26 |
| R103 | 2 M | 0.1\%, 1 w | WW | 54294 | R91-2M | 26 |
| R104 | 2 M | 0.1\%, 1 w | WW | 54294 | R91-2M | 26 |
| R105 | 2 M | 0.1\%, 1 w | WW | 54294 | R91-2M | 26 |
| R106 | $200 \Omega$ | 10\%, 2 w | WWVar | 71450 | RP3-200 | 26 |
| R107 | $100 \mathrm{k} \Omega$ | 0.1\%, 1 w | WW | 54294 | R90-100K | 26 |
| R108 | $* 1 \mathrm{k} \Omega$ | 1\%, 1/2 w | Comp | 00327 | R12-1K | 26 |

[^2]```
00011 Sylvania Electric Products, Inc.
        Buffalo Operations of Sylvania
    Electronic Systems
    Buffalo, N. Y.
0 0 3 2 7 \text { Welwyn International, Inc.}
    Cleveland, Ohio
01121 Allen-Bradley Corp.
    Milwaukee, Wis.
01295 Texas Instruments, Inc.
        Semi-Conductor-Components Division
        Dallas, Texas
01686 RCL Electronics, Inc.
    Riverside, N. J. }71450\mathrm{ CTS Corp.
02735 RCA Semiconductor and Materials
    Division of Radio Corp, of America
    Somerville, N. J.
02777 Hopkins Engineering Co.
    San Fernando, Calif.
04713 Motorola, Inc.
    Semiconductor Products Division
    Phoenix, Arizona
08520 Electronic Devices, Inc.
    North Ridgeville, Ohio
08804 Lamp Metals and Components
    Department G. E. Co.
    Cleveland, Ohio
12065 Transitron Electronic Corp.
    East Boston, Mass.
13050 Potter Co.
    Wesson, Miss.
14655 Cornell-Dubilier Electric Corp.
    Newark, N. J.
15909 Daven Co.
    Livingston, N. J.
24655 General Radio Co.
    West Concord, Mass.
37942 Mallory, P. R., and Co., Inc.
    Indianapolis, Ind.
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        Elkhart, Ind.
    TABLE 7 (Sheet 1). Code List of Suggested Manufacturers; (Based on Federal Supply Code for Manufacturers, Cataloging Handbook H4-1.)

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91637 Dale Electronics, Inc. Columbus, Nebr.
96733 San Fernando Electric Mfg. Co. San Fernando, Calif.
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91737 Gremar Mfg. Co., Inc Wakefield, Mass.

TABLE 7 (Sheet 2). Code List of Suggested Manufacturers. (Based on Federal Supply Code for Manufacturers, Cataloging Handbook H4-1.)

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[^0]:    *Nominal value, factory selected

[^1]:    *Nominal value, factory selected

[^2]:    *Nominal value, factory selected

